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Sensitivity analysis of atmospheric spectral irradiance model

André Albino^{1,*}, Daniele Bortoli¹, Mouhaydine Tlemçani¹, Abdeloawahed Hajjaji², and António Joyce³

¹ Institute of Earth Sciences, University of Évora

² Science Engineer Laboratory for Energy (LabSIPE), National School of Applied Sciences, University of Chouaib Doukkali, Morocco

³ Energy Laboratory, Solar Energy Unit National Laboratory of Energy and Geology

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Abstract. Many radiative transfer models (RTM) have been developed to simulate and estimate solar irradiance. Its accuracy is well documents in literature nonetheless the effect of uncertainties of the parameters on the established model has not been well studied yet. This work focuses on implementing an RTM based on the models found in the literature along with some updates, with the aim to study the sensitivity of the model towards the inputs parameters. The parameters study in this paper are: the Day of year, the Solar zenith angle, the Local atmospheric pressure, the Local temperature, the Relative humidity, the Height of ozone layer concentration, the ozone concentration, the single scattering albedo, the Ground albedo, the Ångström's exponent and the aerosol optical depth. The sensibility analysis is achieved by using the Normalized Root Mean Square Error (NRMSE) as an objective function, calculated with a set of simulated measurements of spectral global solar irradiance and a reference spectrum generated with a group of standard input parameters.

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1 1 Introduction

Solar irradiance spectrum is important in many fields of 2 life sciences (human health, atmospheric sciences, energy). 3 One of the common features of these sciences topics is 4 to perform studies aiming to quantify the uncertainties of 5 the measured solar irradiance [1,2]. The first step to assess these measurements errors is the use of a Radiative trans-7 fer models (RTM) to simulate spectral irradiance for a 8 set of atmospheric representative parameters and boundq ary conditions. Many RTMs have been developed, some 10 of them can be found in [3,4], a couple of commonly used 11 are libradtran [5] and SMART [6]. RTMs are used for pro-12 viding information when measurements are not available, 13 to predict the weather conditions, to help with spectral 14 information in calibrations [7] and to retrieve atmospheric 15 proprieties [8,9]. The accuracy of the RTMs is documented 16 in several studies [3,4,10,11]. Nevertheless, few of them 17 take in account the effect of input uncertainties on the 18 output result [12-16]. 19

This work implements a simple RTM and performs the 20 sensitivity analysis of the implemented model towards 21 each of the input parameters. The model's parameters 22 evaluated are: the day of the year (n), solar zenith angle 23 (θ) , local atmospheric pressure (P), local temperature 24 (T), relative humidity (RH), height of ozone layer concen-25 tration (z_3) , ozone concentration (C_{O_3}) , single scattering 26 albedo (w_0) , ground albedo (ρ_q) , Ångström's exponent (α) 27 and the aerosol optical depth (AOD). This paper seeks to 28

analyses the effect of uncertainties on model inputs in the 29 spectral global radiation estimated by the RTM to better 30 understand the response of the model. Contrasting with 31 the previous published works [12-16] referring to a spe-32 cific region or country, this work uses simulated data with 33 the aim of analyzing the RTM and its response regard-34 less to a specific region. Using real data, the uncertainty 35 depends on all the inputs and the sensors used to measure 36 the parameters, while in simulation uncertainty over each 37 input parameter can be controlled. The analysis is done 38 only one parameter at each time, in order to assess the 39 effect of each one. If all the input parameters are analyzed 40 grouped it should be quite impossible to understand the 41 effect of each one. Results contribute also to show the 42 importance of the measure quality of each parameter. 43

This study is divided into five sections including this introduction. The next section presents the radiative transfer model and its parameters, followed by methodology presentation where the sensitive analysis of each parameter is explained. The fourth section presents and analyses the results obtained. In the finally section the conclusions are introduced.

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2 Radiative transfer model

In this work the implementation of a RTM based on the algorithm established by Iqbal [17] is presented.

The flowchart of the model is depicted in Figure 1. This RTM simulates irradiance for cloudless sky and generates direct, diffuse and global spectral irradiance.

^{*}e-mail: aalbino@uevora.pt

model



Fig. 1. Simplified flowchart of the radiative transfer model.

In the geometric part of the RTM, the eccentricity of 57 the earth's orbit is calculated by [15,17] 58

$$\epsilon = 1 + 0.033 \cos\left(\frac{2\pi n}{365}\right). \tag{1}$$

With the equation (1), extraterrestrial solar spectral 59 irradiance (I_{0n}) can be corrected to the specific day. For 60 the atmospheric composition, the relative optical air mass, 61 the relative optical water-vapor mass and the relative 62 optical ozone mass are estimated. 63

Regarding the atmospheric transmittances, the 64 Rayleigh scattering, the diffusion of uniformly mixed 65 gases, water-vapor and ozone are estimated. The aerosol 66 transmittance is retrieved using Ångström's turbidity for-67 mula. All the transmittances are united in a transmittance 68 due to the combined effects of continuum attenuation and 69 molecular absorption (τ_{λ}) and used to calculate the spec-70 tral direct solar irradiance on the horizontal surface by 71 the Beer-Lambert-Bouguer Law [17] 72

$$I_{d\lambda} = I_{0n} \tau_{\lambda} \cos\left(\theta\right) \tag{2}$$

Finally, the components diffuse and global, of solar 73 irradiance are calculated. 74

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Symbol	Name	Unit
\overline{n}	Day of year	[]
θ	Solar zenith angle	[°]
P	Local atmospheric pressure	[kPa]
w	Precipitable water	[cm]
z_3	Height of ozone layer concentration	[km]
C_{O_3}	Ozone concentration	[DU]
w_0	Single scattering albedo	[]
$ ho_g$	Ground albedo	[]
α	Ångström's exponent	[]
β	Ångström's turbidity coefficient	[]

Table 1. Inputs parameters used by radiative transfer

Using the interpolation method, different wavelength

step can be used. Some parts of the model were updated using different data and more detailed equations from recent studies [18–20]. Extraterrestrial Solar Spectral Irradiance was modified using the data from Gueymard [18]. The ozone attenuation coefficients are replaced with the cross-section of ozone determined by by Bogunil et al. [19]. The equation presented by Frohlich and Shaw for Rayleigh optical depth (ROD) [20], was also used:

$$ROD = -0.00838\lambda^{-3.916 - 0.074\lambda - \frac{0.050}{\lambda}}$$
(3)

where λ is the wavelength in nm. The RTM use ten inputs to describe the atmospheric state, present in Table 1.

Some of the considered quantities are difficult to measure or to obtain. However, they can be estimated using other proprieties: in this work we estimated the values for the precipitable water (w) and the Ångström's turbidity coefficient (β). This is done using the equation of Leckner [17,21] which is based on the local temperature (T) and the relative humidity (RH)

$$v = \frac{0.493 \times RH \times p_s}{T} \tag{4}$$

where p_s is the partial pressure of water vapor in saturated air and is given by

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$$p_s = exp\left(26.23 - \frac{5416}{T}\right) \tag{5}$$

The Ångström's turbidity coefficient can be calculated from Angström's Law [4], knowing the Angström's exponent and the aerosol optical depth (AOD) at one wavelength (λ_0)

$$\beta = AOD_{(\lambda_0)}\lambda_0^{\alpha}.$$
 (6)

3 Methodology

To study the effect of the input parameters uncertainty on 101 the established model, a set of inputs is fixed in order to be 102 the standard parameters values, this values are present in 103 Table 2. Their application to the model generates a stan-104 dard spectral irradiance (Istd) starting in 0.325 μ m and 105 finish at 1.075 μ m with a step of 1 nm. Following this 106

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 Table 2. Standard input values

Input parameter	Value
\overline{n}	182
θ	45 °
P	101 kPa
T	$25^{\circ}\mathrm{C}$
RH	50%
z_3	20 km
C_{O_3}	300 DU
w_0	0.5
$ ho_g$	0.5
α	1.5
$AOD_{(\lambda_0)}$	0.1
λ_0	$0.675~\mu{ m m}$

step, the selected parameters are sequentially modified. 107 Pressure (P), temperature (T), Height of ozone layer con-108 centration (z_3) , Ozone concentration (C_{O_3}) , Angström's 109 exponent (α) and Aerosol optical depth (AOD) range 110 from 50% to 150% of the standard values with a step 111 of 0.01%. In the rest of the parameters, all their range 112 has analyzed. Single scattering albedo (w_0) and Ground 113 albedo (ρ_a) change between 0 and 1, Relative humidity 114 (RH) between 0 and 100 %, Solar zenith angle range from 115 0 to 90° and the Day of year from 1 to 365. Using these 116 new values, the output of the model (I) is evaluated 1000 117 times, generating a new set of solar irradiances. White 118 noise is added to this set, in order to produce a more 119 realistic simulation measurements of solar radiation. The 120 used white noise has mean value sets at zero and stan-121 dard deviation of 1%. With the new obtained irradiance 122 values, the normalized root mean square error (NRMSE) 123 is calculated as shown in equation (7)124

NRMSE =
$$100 \frac{\sqrt{\frac{\sum (I_{std} - I)^2}{n}}}{\max(I) - \min(I)}$$
. (7)

The mean and standard deviation values of NRMSE of 125 each parameter is calculated and plotted versus the nor-126 malized variation of the parameter. Through the plots, 127 the sensitivity of the model to each parameter can be 128 observed, i.e., if an error on the input parameter occurs, 129 it is reflected by an increase or decrease in the output of 130 the model. The used standard input values are shown 131 in Table 2. The global solar irradiance spectrum gen-132 erated by the RTM with standard values is present in 133 Figure 2. 134

135 4 Results

This section presents the plots of NRMSE for each input 136 parameter. The first parameter analyzed is the day of 137 year, present in Figure 3. The influence of the day of 138 year on the model has been observed, is possible to see 139 the seasonality of irradiance. The day chosen to be the 140 standard value for the day of year was 182 – July 1 –, 141 it is in the beginning of summer. The nearest days have 142 showed a small error -0.75% – and, in oppose, the higher 143 error -4.83% – was detected in the winter, like expected. 144



Fig. 2. Simulated global solar radiation spectrum generated with the radiative transfer model in the standard condition present in Table 2. The spectrum range from 0.325 to $1.075 \,\mu\text{m}$ with a step of 1 nm.



Fig. 3. Mean value (line) and standard deviation (gray area) of Normalized Root Mean Square of the output of the model with the day of year.

The standard deviation of NRMSE (gray area in plot) ¹⁴⁵ increase with distance of the standard value of the day of ¹⁴⁶ year. ¹⁴⁷

The next analyzed parameter is the solar zenith angle 148 (θ) , which can be seen in Figure 4. This is the most influ-149 encer parameter on the model. When the θ is 90° the 150 mean error go to 567% with a standard deviation of 3.4%. 151 On the other hand, when θ go to 0° the error is small 152 than the previous – stay 22% – with a deviation of 0.18%. 153 Even so the highest error cause by a input parameter 154 of model. The main reason for this error is the influence 155 of solar zenith angle in the estimation of relative optical 156 air mass. The relative optical air mass is estimated by 157 the formulation of Kasten (Eq. (8)) [17] which present a 158



Fig. 4. Mean value (line) and standard deviation (gray area) of Normalized Root Mean Square of the output of the model with the solar zenith angle.



Fig. 5. Mean value (line) and standard deviation (gray area) of Normalized Root Mean Square of the output of the model. In the lower axis the local atmospheric pressure variation is present in percentage while in the upper axis this presents the local atmospheric pressure in kPa.

significant error for angles greater than 86 $^{\circ}$.

$$m_r = \left[\cos\theta + 0.15 \left(93.885 - \theta\right)^{-1.253}\right]^{-1}.$$
 (8)

The local atmospheric pressure shown in Figure 5, 160 presents a symmetric NRMSE, i.e., nearly the same error 161 on both sides of the standard pressure value regardless 162 of if the variation is to greater or lower values. The error 163 increases until near 7% at the boundary values. It can also 164 be noticed that the standard deviation value increases 165 with the distance to the reference value, from 0.02% to 166 0.08%.167



Fig. 6. Mean value (line) and standard deviation (gray area) of Normalized Root Mean Square of the output of the model. In the lower axis the local temperature variation is present in percentage while in the upper axis this presents the local temperature in $^{\circ}C$.

Almost symmetric is the error on the output of the model generated by the local temperature, as can be seen in Figure 6. To the highest temperature study $(37.5 \,^{\circ}\text{C})$ mean error is 2.05%, a little lower than error to the smallest temperature $(12.5 \,^{\circ}\text{C}) 2.23\%$. The standard deviation of the NRMSE present a small negative correlation with temperature. The standard deviation of the error is 0.02% at the 25 $^{\circ}\text{C}$.

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The next parameter to be analyzed is the relative humidity, and all range was study. The reference value used is 50% and in Figure 7 can be see that an error to a dry condition is almost 7%. To moist condition the mean error is three and half times less, around 2%. Standard deviation follow the similar shape, higher to dry and smaller to moist condition.

The curve of the height of ozone layer concentration, in Fig. 8, shows that the model is almost not influenced by this parameter. The change in the mean value of the NRMSE is very small. In this case the noise can be more important than the variation of the parameter

The effect of the Ozone concentration on the model is 188 depicted in Figure 9. In this plot, it can be seen that an 189 error of 50% in the input ozone concentration relatively 190 to the standard value – 300 DU – will produce an approx-191 imative NRMSE of 1.3%. Also the plot show a shape of 192 the NRMSE is very symmetric. This curve denote that 193 this parameter does not have a "preferential side", i.e., 194 the NRMSE varies the same way on either side of the 195 standard value. The error in output increases with the 196 error in input as expected. The standard deviation also 197 increases with the input error, its value at standard ozone 198 concentration is 0.02% and increase to 0.03%. 199

The next parameter to be analyzed is the single scattering albedo. The maximum error is near 10% when the parameter go to zero. The standard deviation follows the



Fig. 7. Mean value (line) and standard deviation (gray area) of Normalized Root Mean Square of the output of the model with the variation of the relative humidity.



Fig. 8. Mean value (line) and standard deviation (gray area) of Normalized Root Mean Square of the output of the model. In the lower axis the variation of heigth of ozone layer concentration in percentage is presents while in the upper axis this presents the heigth of ozone layer concentration in km.

same pattern that the mean value of NRMSE, increasing
with the increase of the variation, like it can be seen in
Figure 10.

The variation of ground albedo is very symmetric and 206 presents a maximum error of 4% to the limits of is range. 207 The standard deviation present the same shape of the 208 mean value. The standard deviation of the error to the 209 standard value of this parameter -0.5 – is around 0.02%210 and ends near 0.05% to the extreme values. The graph of 211 the NRMSE in function of ground albedo can be seen in 212 Figure 11. 213



Fig. 9. Mean value (line) and standard deviation (gray area) of Normalized Root Mean Square of the output of the model. In the lower axis the ozone concentration variation is present in percentage while in the upper axis this presents the Ozone concentration in DU.



Fig. 10. Mean value (line) and standard deviation (gray area) of Normalized Root Mean Square of the output of the model with the variation of the single scattering albedo.

Figure 12 presents the NRMSE in function of the vari-214 ation of the Ångström's exponent. It is visible that, to an 215 Ångström's exponent of 2.25, NRMSE will be around 3%. 216 To other side to a variation of 50% of the standard value 217 -1.5 – the mean value is higher than 2%. This parameter 218 is more responsive to variations to values higher than the 219 standard value of the Ångström's exponent. Relatively to 220 the standard deviation, it is, also, increasing faster to the 221 higher value of the parameter analyzed and slower to the 222 smaller value. 223

Finally, the last parameter to study, is the aerosol optical depth at the 0.675 µm wavelength. The aerosol optical 225



Fig. 11. Mean value (line) and standard deviation (gray area) of Normalized Root Mean Square of the output of the model with the variation of the ground albedo.



Fig. 12. Mean value (line) and standard deviation (gray area) of Normalized Root Mean Square of the output of the model. In the lower axis the Ångström's exponent variation is present in percentage while in the upper axis this presents the Ångström's exponent.

depth generates similar mean NRMSE to higher and lower values of the parameter than the standard value -0.1. The higher value of the mean NRMSE is around 3.6% to the extreme values, and the lowest value -0.75% – at the standard value. Standard deviation are very symmetric present values near 0.05% to the range limits and 0.02%to the standard values.

233 5 Conclusion

The analysis performed in this work allows to see the influence of the errors and uncertainties of the input



Fig. 13. Mean value (line) and standard deviation (gray area) of Normalized Root Mean Square of the output of the model. In the lower axis the variation of aerosol optical depth at the 0.675 μ m is present in percentage while in the upper axis this presents the aerosol optical depth at the 0.675 μ m.

parameters on the output of the radiative transfer model. 236 This study shows that the main parameters which influ-237 ence the output of the model are the solar zenith angle 238 with an error higher of 600%, the local single scatter-239 ing albedo with an error near 10% and with near 7%240 mean error the local atmospheric pressure and the rela-241 tive humidity. In part, the error cause in the model output 242 by solar zenith angle can be explained by the formula-243 tion of Kasten to relative optical air mass and its error 244 to large angles. More information can be withdrawal from 245 this study. Using the obtained graphs, it can now be possi-246 ble to approximate the initial parameters knowing if they 247 should be underestimated or overestimated. This analy-248 sis also shows that the height of ozone layer concentration 249 can be used as a constant, one time that its error is always 250 equal. 251

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